

A PULSE TUBE REFRIGERATOR

Field of the invention

The present invention relates to pulse tube refrigerators for
5 recondensing cryogenic liquids. In particular, the present invention
relates to the same for magnetic resonance imaging systems.

Background to the Invention

In many cryogenic applications components, e.g. superconducting
10 coils for magnetic resonance imaging (MRI), superconducting
transformers, generators, electronics, are cooled by keeping them in
contact with a volume of liquefied gases (e.g. Helium, Neon, Nitrogen,
Argon, Methane). Any dissipation in the components or heat getting
into the system causes the volume to part boil off. To account for the
15 losses, replenishment is required. This service operation is considered
to be problematic by many users and great efforts have been made over
the years to introduce refrigerators that recondense any lost liquid right
back into the bath.

As an example of prior art, an embodiment of a two stage Gifford
20 McMahan (GM) coldhead recondenser of an MRI magnet is shown in
Figure 1. In order for the GM coldhead, indicated generally by 10, to be
removable for service or repair, it is inserted into a sock, which connects
the outside face of a vacuum vessel 16 (at room temperature) to a helium
bath 18 at 4K. MRI magnets are indicated at 20. The sock is made of
25 thin walled stainless steel tubes forming a first stage sleeve 12, and a
second stage sleeve 14 in order to minimise heat conduction from room

temperature to the cold end of the sock operating at cryogenic temperatures. The sock is filled with helium gas 30, which is at about 4.2 K at the cold end and at room temperature at the warm end. The first stage sleeve 12 of the coldhead is connected to an intermediate heat station of the sock 22, in order to extract heat at an intermediate temperature, e.g. 40K-80 K, and to which sleeve 14 is also connected. The second stage of the coldhead 24 is connected to a helium gas recondenser 26. Heat arises from conduction of heat down through the neck, heat radiated from a thermal radiation shield 42 as well as any other sources of heat for example, from a mechanical suspension system for the magnet, (not shown) and from a service neck (also not shown) used for filling the bath with liquids, instrumentation wiring access, gas escape route etc. The intermediate section 22 shows a passage 38 to enable helium gas to flow from the volume encircled by sleeve 14. A number of passages may be annularly distributed about the intermediate section. The latter volume is also in fluid connection with the main bath 36 in which the magnet 20 is placed. Also shown is a flange 40 associated with sleeve 12 to assist in attaching the sock to the vacuum vessel 16. A radiation shield 42 is placed intermediate the helium bath and the wall of the outer vacuum vessel.

The second stage of the coldhead is acting as a recondensor at about 4.2 K. As it is slightly colder than the surrounding He gas, gas is condensed on the surface (which can be equipped with fins to increase surface area) and is dripped back into the liquid reservoir. Condensation locally reduces pressure, which pulls more gas towards the second stage. It has been calculated that there are hardly any losses due to natural

convection of Helium, which has been verified experimentally provided that the coldhead and the sock are vertically oriented (defined as the warm end pointing upwards). Any small differences in the temperature profiles of the Gifford McMahon cooler and the walls would set up gravity assisted gas convection, as the density change of gas with temperature is great (e.g. at 4.2 K the density is 16 kg/m^3 ; at 300 K the density is 0.16 kg/m^3). Convection tends to equilibrate the temperature profiles of the sock wall and the refrigerator. The residual heat losses are small.

When the arrangement is tilted, natural convection sets up huge losses. A solution to this problem has been described in US Patent, US-A-5,583,472, to Mitsubishi. Nevertheless, this will not be further discussed here, as this document relates to arrangements which are vertically oriented or at small angles ($< 30^\circ$) to the vertical.

It has been shown that Pulse Tube Refrigerators (PTRs) can achieve useful cooling at temperatures of 4.2 K (the boiling point of liquid helium at normal pressure) and below (C. Wang and P.E. Gifford, Advances in Cryogenic Engineering, 45, Edited by Shu et al., Kluwer Academic/Plenum Publishers, 2000, pp. 1-7). Pulse tube refrigerators are attractive, because they avoid any moving parts in the cold part of the refrigerator, thus reducing vibrations and wear of the refrigerator. Referring now to Figure 2, there is shown a PTR 50 comprising an arrangement of separate tubes, which are joined together at heat stations. There is one regenerator tube 52, 54 per stage, which is filled with solid materials in different forms (e.g. meshes, packed spheres, powders). The materials act as a heat buffer and exchange heat with the working

fluid of the PTR (usually He gas at a pressure of 1.5-2.5 MPa). There is one pulse tube 56, 58 per stage, which is hollow and used for expansion and compression of the working fluid. In two stage PTRs, the second stage pulse tube 56 usually links the second stage 60 with the warm end 62 at room temperature, the first stage pulse tube 58 linking the first stage 64 with the warm end.

It has been found, that PTRs operating in vacuum under optimum conditions usually develop temperature profiles along the length of the tubes that are significantly different one tube to another in the same temperature range and also from what would be a steady state temperature profile in a sock. This is shown in Figure 3.

Another prior art pulse tube refrigerator arrangement is shown in Figure 4 wherein a pulse tube is inserted into a sock, and is exposed to a helium atmosphere wherein gravity induced convection currents 70, 72 are set up in the first and second stages. The PTR unit 50 is provided with cold stages 31, 33 which are set in a recess in an outer vacuum container 16. A radiation shield 42 is provided which is in thermal contact with first sleeve end 22. A recondenser 26 is shown on the end wall of second stage 33. If at a given height the temperatures of the different components are not equal, the warmer components will heat the surrounding helium, giving it buoyancy to rise, while at the colder components the gas is cooled and drops down. The resulting thermal losses are huge, as the density difference of helium gas at 1 bar changes by a factor of about 100 between 4.2 K and 300 K. The net cooling power of a PTR might be e.g. 40 W at 50 K, and 0.5 W to 1 W at 4.2 K. The losses have been calculated to be of the order of 5-20 W. The

internal working process of a pulse tube will, in general, be affected although this is not encountered in GM refrigerators. In a PTR, the optimum temperature profile in the tubes, which is a basis for optimum performance, arises through a delicate process balancing the influences of many parameters, e.g. geometries of all tubes, flow resistivities, velocities, heat transfer coefficients, valve settings etc. (A description can be found in Ray Radebaugh, proceedings of the 6th International Cryogenic Engineering Conference, Kitakyushu, Japan, 20-24 May, 1996, pp. 22-44).

Therefore, in a helium environment, PTRs do not necessarily reach temperatures of 4 K, although they are capable of doing so in vacuum. Nevertheless, if the PTR is inserted in a vacuum sock with a heat contact to 4 K through a solid wall, it would work normally. Such a solution has been described for a GM refrigerator (US Patent US-A-5,613,367 to William E. Chen, GE) although the use of a PTR would be possible and be straightforward. The disadvantage, however, is that the thermal contact of the coldhead at 4 K would produce a thermal impedance, which effectively reduces the available power for refrigeration. As an example, with a state of the art thermal joint made from an Indium washer, a thermal contact resistance of 0.5 K/W can be achieved at 4 K (see e.g. US-A-5,918,470 to GE). If a cryocooler can absorb 1 W at 4.2 K (e.g. the model RDK 408 by Sumitomo Heavy Industries) then the temperature of the recondensor would rise to 4.7 K, which would reduce the current carrying capability of the superconducting wire drastically. Alternatively, a stronger cryocooler

would be required to produce 1 W at 3.7 K initially to make the cooling power available on the far side of the joint.

Figure 5 shows an example of such a PTR arrangement 76. The component features are substantially the same as shown in Figure 4.
5 Thermal washer 78 is provided between the second stage of the PTR coldhead and a finned heat sink 26. A helium-tight wall is provided between the thermal washer and the heat sink.

Object of the invention

10 The present invention seeks to provide an improved pulse tube refrigerator.

Statement of the Invention

In accordance with a first aspect of the invention, there is
15 provided a pulse tube refrigerator PTR arrangement within a cryogenic apparatus, wherein a regenerator tube of a PTR is finned. Ideally, there is a plurality of fins. The fins conveniently comprise annular discs and are spaced apart along the length of the regenerator tube. Alternatively the fins comprise outwardly directed fingers or prongs. The fins may
20 also comprise a single spiral arrangement. Conveniently, an associated sock surrounds all the tubes of the pulse tube, leaving only a small annular gap between the regenerator and pulse tubes and a wall of the sock. The walls of the tubes can be fabricated from materials such as thin gauge stainless steel or alloys.

25 The invention provides a regenerator for a PTR which can act as a distributed cooler, that is to say that there is refrigeration power along

the length of the regenerator. This means that the regenerator can intercept (absorb) some of the heat being conducted down the refrigerator sock (neck tube, helium column plus other elements). Whilst the absorption of this heat degrades the performance of the second stage, in one sense, this degradation is less than the heat which is extracted (intercepted) by the regenerator and therefore there is a net gain in cooling power. By placing fins along the regenerator the distributed cooling power of the regenerator is increased by enhancing the heat transfer (by increasing the surface area available for the transfer) to the helium column (and therefore the neck tube etc) that is to say, the fins or baffles, are believed to increase the surface area available for distributed heat transfer from the helium atmosphere to the regenerator.

15 Brief description of the figures

The invention may be understood more readily, and various other aspects and features of the invention may become apparent from consideration of the following description and the figures as shown in the accompanying drawing sheets, wherein:

20 Figure 1 shows a two stage Gifford McMahon coldhead recondenser in a MRI magnet;

Figure 2 shows a PTR consisting of an arrangement of separate tubes, which are joined together at the heat stations;

Figure 3 shows a temperature profile in a sock;

25 Figure 4 shows a pulse tube inserted into a sock;

Figure 5 shows a prior art example of a pulse tube with a removable thermal contact;

Figure 6 shows a first embodiment of the invention;

Figure 6A shows a cross-section of a regenerator tube of the first
5 embodiment;

Figures 7A-G shows various forms of regenerator tubes; and

Figures 8-10 show further variations of the invention.

Detailed description of the invention

10 There will now be described, by way of example, the best mode contemplated by the inventors for carrying out the invention. In the following description, numerous specific details are set out in order to provide a complete understanding of the present invention. It will be apparent, however, to those skilled in the art, that the present invention
15 may be put into practice with variations from the specific embodiments.

Referring now to Figure 6, there is shown a first embodiment of the invention, wherein a 2-stage PTR arrangement 90 is shown. Regenerator tubes 92, 94 and pulse tubes 96, 98 are shown with regenerator tube 94 being finned.

20 Figure 6A shows a cross-section through the regenerator tube 94 showing annular fin 104 surrounding tube 94 in the form of an annular disc. Conveniently the tube wall and the fins are manufactured simultaneously, preferably from the same material which is moderately thermally conductive, such as an austenitic stainless steel. Other
25 materials that could be used include brass and aluminium alloys. However, if the component materials of the fins and tube are different,

then it is preferable that the fins are made of a material that is highly thermally conductive and that the tube is made of a material that is moderately thermally conductive. For low pressure PTRs, it would be possible to employ a composite material, which materials can be
5 moderately thermally conductive, and provide fins made from copper or some other highly thermally conductive material, which would be bonded to the composite. It is to be noted that pure metals can be highly thermally conductive at low temperatures.

The fins should have very good thermal contact with the
10 regenerator which can be achieved by, for example, soldering, welding or brazing. The fins intercept the heat being transferred down the helium columns, neck tube and other elements within the neck. It is believed that the absorption of the heat may degrade the performance of the second stage, although it is believed that this degradation in power is
15 less than the heat extracted by the regenerator and therefore there is a net gain in the available cooling power and thus the recondensation rate of helium gas. The provision of fins increase the distributed cooling due to the enhanced heat transfer with the gas column arising as a result of the increased surface area available. These fins can also be used on the
20 first stage regenerator in order to minimise the heat load from the 300k stage to the first stage. Another advantage for this configuration is that these fins can work as barriers against the natural convection between the high temperature and low temperature levels. Accordingly, the natural convection and its heat load to the second stage may be reduced.

25 In Figures 7A-F, different mechanical forms of the finned tube 94 are shown. In Figure 7A the finning comprises an array of annular discs

120 about a straight tube. The tube wall is thick enough to withstand the surrounding helium pressure during evacuation without any buckling. The fins are conveniently placed at equi-spaced intervals and are preferably of the same dimension.

5 In figure 7B, the fin comprises a spiral tape 122, affixed to the regenerator tube 94". In Figure 7C the fins comprise spikes 126 about tube 94"', in an arrangement somewhat akin to the spikes of a hedgehog. This arrangement would not, however, reduce convection currents about the tube, although would allow easier gas flow past the tube if it was
10 required, for example, during a quench.

In figure 7D the tube 128 is corrugated in an arrangement similar to accordion bellows. In figure 7E plates 130 are placed about tube 94'''; the plates being attached such that they are parallel with the axis of the tube. Tube 132 is corrugated with the axis of corrugation being
15 parallel with the axis of the tube.

The tube of Figure 7F is corrugated with creases arranged parallel with the axis of the tube. In figure 7G the fins comprise annular fins which cover only a portion of the length of the tube. This sort of tube is preferable for the upper sections since, as can be seen with reference to
20 Figure 3, that the temperature of the neck tube and the first regenerator correspond. That is to say to have a first regeneration tube fully finned along its length would be counter-productive to efficient operation.

The fins for individual tubes can differ amongst each other. In some applications it may be necessary to provide fins on the first stage
25 and the second stage regenerators. The teaching of the present invention can be applied with the teaching disclosed in the PCT patent application

number PCT/EP02/11882. In other words, in addition to the regeneration tubes having fins to aid heat conduction through the tube walls, the pulse tubes may be insulated to reduce heat conduction through the tube walls.

5 Figure 8 shows pulse tubes 101, 103 with insulating sleeves and regeneration tube 94 with fins 104. Figure 9 shows only pulse tube 101 with an insulating sleeve and regeneration tube 94 with fins. Figure 10 shows a similar arrangement to figure 8 except that regeneration tube 92 is also provided with fin 102.

10 While most applications cryogenic temperatures, e.g. at or around 4 K for MRI apparatus operate with two stage coolers, the same technology can also be applied to single stage coolers or three and more stage coolers.

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